

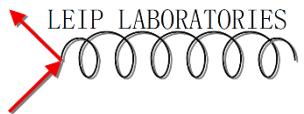


Thermal Neutron Scattering Law Methods and Evaluations

Ayman I. Hawari
Distinguished Professor & Director

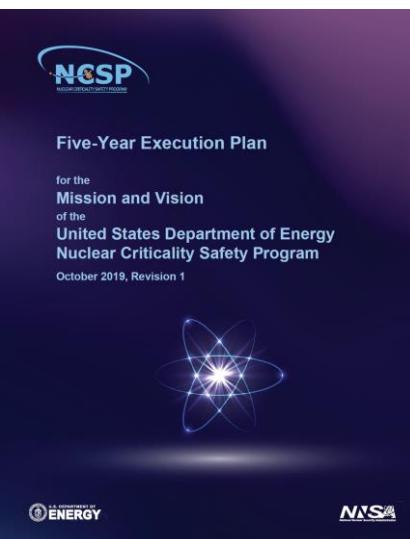
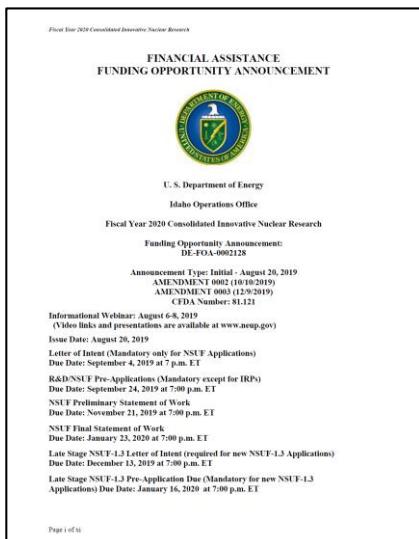
Nuclear Reactor Program
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Raleigh, North Carolina, USA

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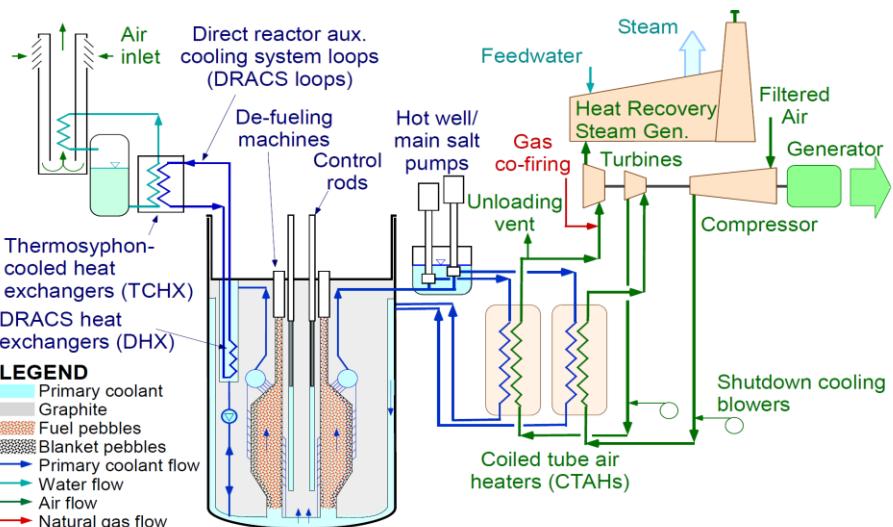
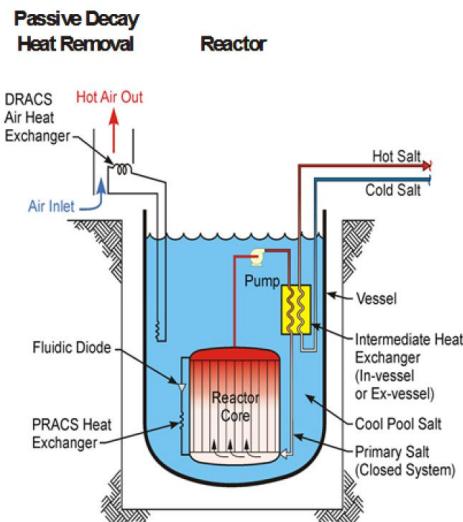
Acknowledgment

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- NNSA Nuclear Criticality Safety Program (NCSP)
 - in collaboration with LLNL
- Naval Nuclear Propulsion Program (NNPP)

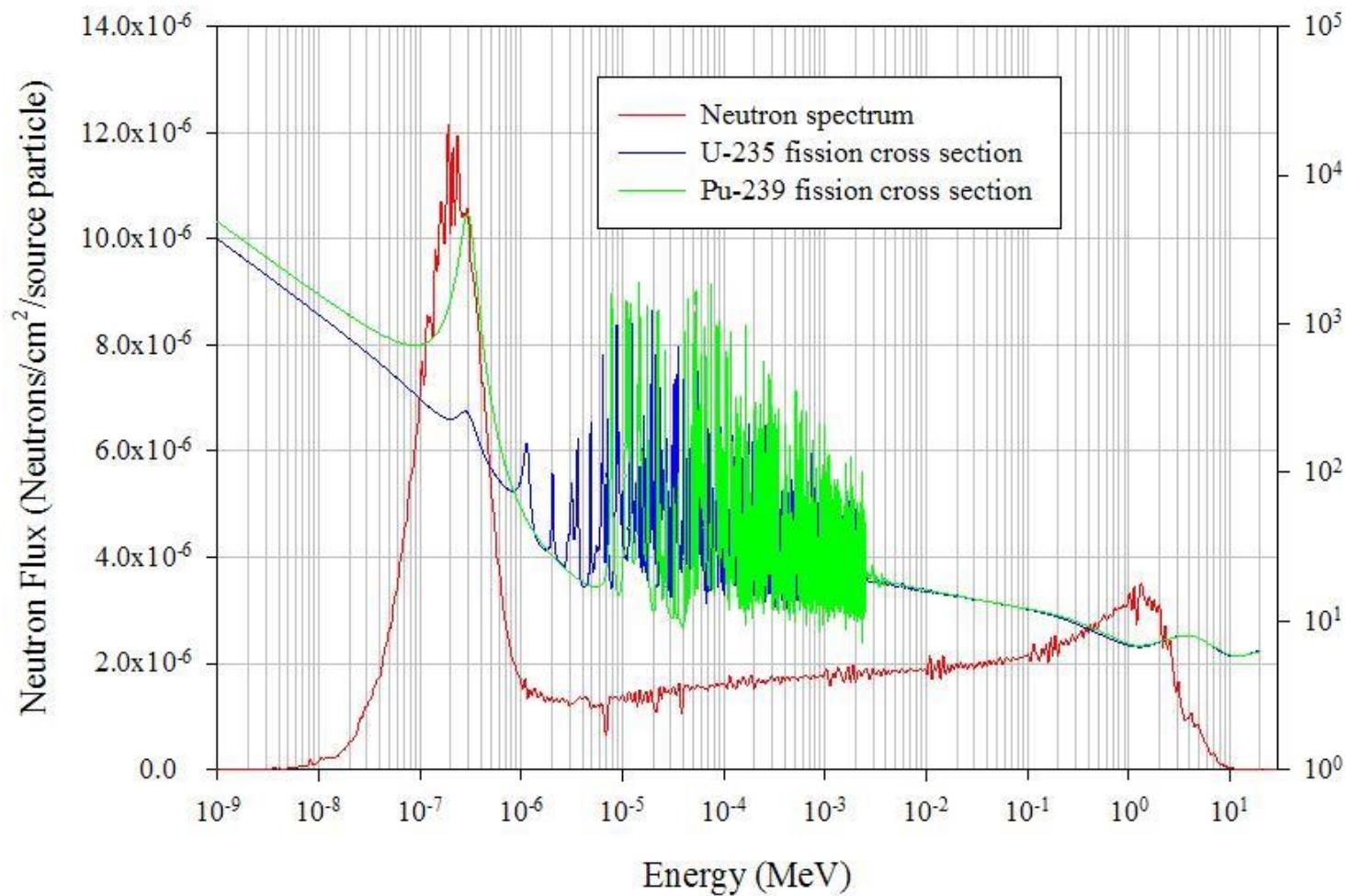


Motivation – Neutronic Systems

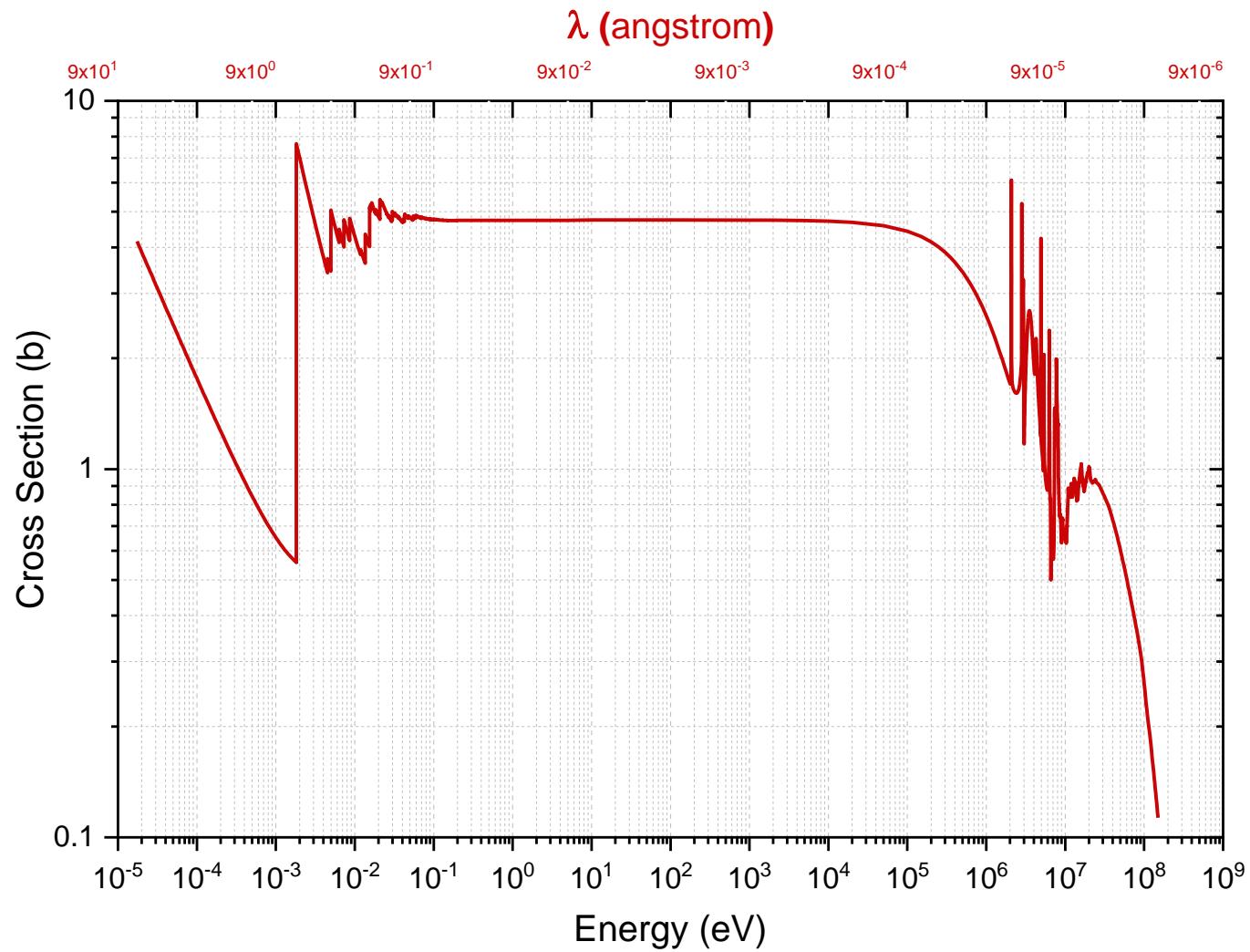
- Several concepts of advanced thermal reactors have been proposed including the LWR, AHTR and FHR
 - The core is dominated by light water, graphite and molten salt moderators



Reactor Characteristics



Neutron Interactions – Carbon



Neutron Thermalization

Using first Born approximation combined with Fermi pseudopotential, it can be shown that the double differential scattering cross section has the form

$$\frac{d^2\sigma}{d\Omega dE'} = \frac{1}{4\pi} \sqrt{\frac{E'}{E}} \left\{ \sigma_{coh} S(\vec{k}, \omega) + \sigma_{incoh} S_s(\vec{k}, \omega) \right\}$$

The scattering law $S(\vec{k}, \omega)$ is composed of two parts

$$S(\vec{k}, \omega) = S_s(\vec{k}, \omega) + S_d(\vec{k}, \omega)$$

Van Hove's space-time formulation

$$I(\vec{k}, t) = \int G(\vec{r}, t) \exp(i\vec{k} \cdot \vec{r}) d\vec{r}$$

$$S(\vec{k}, \omega) = \frac{1}{2\pi\hbar} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} G(\vec{r}, t) e^{i(\vec{k} \cdot \vec{r} - \omega t)} d\vec{r} dt$$

where $G(\vec{r}, t)$ is the *dynamic pair correlation function* and can be expressed in terms of time dependent atomic positions.

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$$S_s(\alpha, \beta) = k_B T \cdot S_s(\vec{\kappa}, \omega)$$

$$\left. \frac{d^2\sigma}{d\Omega dE'} \right|_{inelastic} = \frac{\sigma}{2k_B T} \sqrt{\frac{E'}{E}} S_s(\alpha, \beta)$$

$$\beta = \frac{E - E'}{k_B T} \quad \text{Energy transfer}$$

$$\alpha = \frac{(E + E' - 2\sqrt{EE'} \cos \theta)}{k_B T} \quad \text{Momentum transfer}$$

The scattering law (TSL) is the Fourier transform of a Gaussian correlation function

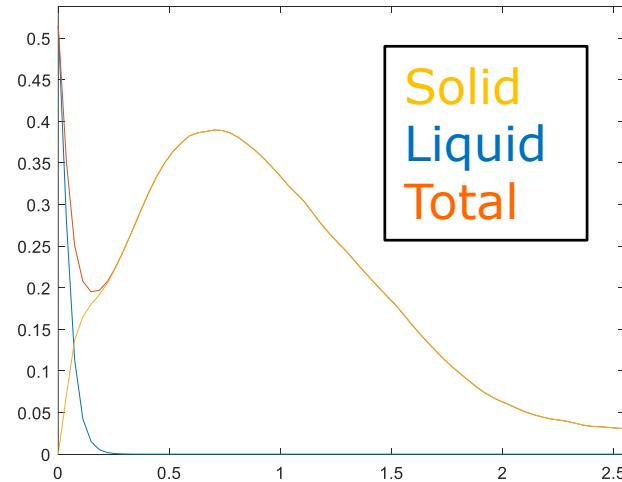
$$S_s(\alpha, \beta) = \frac{1}{2\pi} \int_{-\infty}^{\infty} e^{-i\beta t} e^{-\gamma(t)} dt$$

$$\gamma(t) = \frac{\alpha}{2} \int_{-\infty}^{\infty} \frac{\rho(\beta)}{\beta \sinh(\beta/2)} [1 - e^{-i\beta t}] e^{\beta/2} d\beta$$

$\rho(\beta)$ – density of states (e.g., phonon frequency distribution)

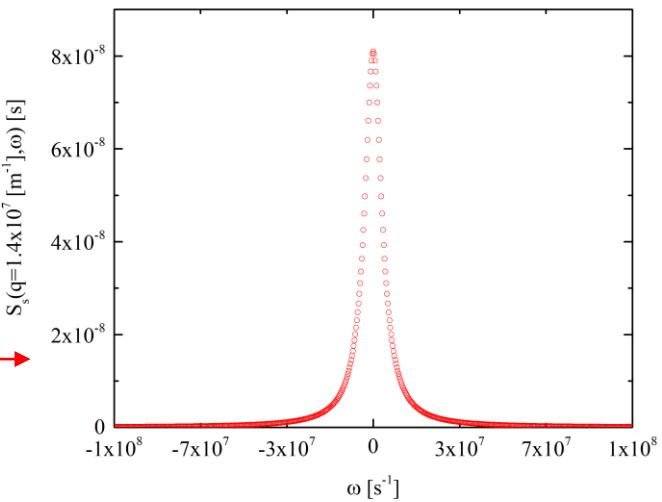
Thermalization in Liquids

- **Separation** of the diffusive DOS from the continuous (solid) DOS



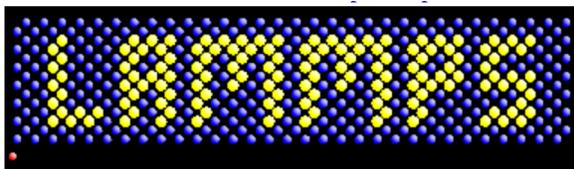
- **Convolution** of the solid and liquid TSL components

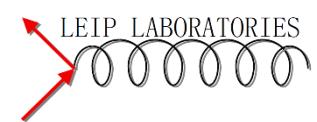
$$S_{total}(\alpha, \beta) = (S_{diff.}(\alpha, \beta) * S_{cont.}(\alpha, \beta))$$



Thermal Scattering Law Analysis

- Key development in the last 20 years is the use of atomistic simulations methods to support the evaluation process
 - Produce data necessary to calculate the TSL including
 - DOS for evaluation of TSL
 - Direct access to TSL using correlation analysis
 - Support computational and experimental analysis





Thermal Scattering Law Analysis

PIFOR 2004: The Physics of Fuel Cycles and Advanced Nuclear Systems: Global Developments
Chicago, Illinois, April 25-29, 2004, on CD-ROM, American Nuclear Society, Laramie Park, IL, (2004)

Ab Initio Generation of Thermal Neutron Scattering Cross Sections

A. I. Hawari, I. I. Al-Qasie, V. H. Gillette, B. W. Weltman, T. Zhou
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Quantum mechanical ab initio (i.e., first principle) methods are applied in generating the thermal neutron scattering cross sections of moderators and reflectors that are of interest in modern technology. Specifically, this work focuses on graphite and beryllium. In both cases, the ab initio code VASP and the lattice dynamics code PHONON were used to generate the dispersion relations, and the phonon frequency distributions (density of states). This information was then utilized in the LEAPW module of the NJOY code to calculate the thermal neutron scattering cross sections at various temperatures. The use of the ab initio approach represents a major departure from previously applied methods, which depended mainly on fitting simpler dynamical models to experimental data to arrive at the phonon frequency distributions. In this case, much more complicated models of the atomic system of interest can be set up, which allows the establishment of a more complete dynamical analysis. As opposed to the semi-empirical methods used previously, this method represents a fundamental and predictive approach for estimating materials' properties including ones that are of interest in nuclear reactor design.

KEYWORDS: neutron, thermal neutron, slow neutron, ab initio, VASP, graphite, beryllium, moderator, phonon frequency distribution, thermal neutron scattering cross section, nuclear reactor

1. Introduction

Due to advances in computational power, the possibility now exists to perform detailed quantum mechanical ab initio (i.e., first principle) simulations of atomic systems. These simulations are currently used in fields such as physics, chemistry, and materials science to characterize and predict the behavior of new and novel materials [1]. Using this approach, it is possible to establish the equilibrium atomic positions of a given system by calculating the forces of interaction that result from both basic information as the coordinates of the atoms. Consequently, ab initio simulations seek to gain insight into the bonding forces in the material, which are usually variations of the Coulomb force that result in the formation of ionic, covalent, metallic, and van der Waals bonds.

In nuclear reactors, the effect of ionic and covalent bonding becomes important as the neutrons slow down and enter the thermal (or slow) region (neutron energy < 1 eV). The microscopic interaction (i.e., absorption, scattering, etc.) of slow neutrons within the reactor core defines the thermal neutron energy spectrum, which affects several global (macroscopic) properties such as criticality, safety and feedback response. Therefore, the accuracy of the thermal neutron scattering cross sections that are used in reactor core design calculations are important for operating the reactor in an optimized and safe manner.

In the past, the thermal neutron scattering cross sections were derived from structure dynamics models that were fitted to experimental data in order to quantify the forces between the atoms and calculate the required excitation density of states [2]. However, by using the ab initio approach, the ability now exists to treat much larger systems of atoms, and arrive at more accurate and complete dynamical models from



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Modern Techniques for Inelastic Thermal Neutron Scattering Analysis

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A predictive approach based on ab initio quantum mechanics and/or classical molecular dynamics simulations has been formulated to calculate the scattering law, $S(\vec{k}, \omega)$, and the thermal neutron scattering cross section, $\sigma_{\text{th}}(\vec{k}, \omega)$. This approach is able to generate the inelastic thermal neutron scattering cross sections of any material and to accurately reflect the physical conditions of the medium (i.e., temperature, pressure etc.). In addition, the approach is able to generate the scattering cross sections using the Born approximation theory and, in the case of solids, crystalline perfection. As a result, new and improved thermal neutron scattering cross sections are generated for a wide range of materials. These materials include materials used for reactor moderators and reflectors such as reactor-grade graphite and beryllium. The approach is also able to generate the thermal neutron scattering cross sections for materials such as solid methane, and neutron beam filters such as sulphur and bismuth. Consequently, it is anticipated that the above approach will play a major role in providing the nuclear science and engineering community with a better understanding of the physical properties of materials when experimental information may be scarce or nonexistent.

1. INTRODUCTION

Low energy ("thermal") neutrons are characterized by energies that are on the order of the excitation (ionization, rotation etc.) energy in the medium in which they interact. Furthermore, their de Broglie wavelength is comparable to the size of the atoms. Consequently, such neutrons are highly sensitive to the atomic bonding details of the system that surrounds them including the interactions between the incident neutron's atoms and the neutrons. The scattering and dynamical properties of the atomic system are usually obtained by scattering methods. The scattering of low energy neutrons in an atomic system is governed by the Fermi pseudopotential and the presence (coherent) effects. Examination of Eq. 1 shows that the thermal neutron scattering cross section depends on three factors: first, the ratio of the scattering and inelastic scattering cross sections, and second, the ratio of the bound atom cross sections, and third, a factor that represents the dynamics of the scattering law. The last factor is the ratio of the scattering law to the scattering law.

From the calculation of the thermal scattering cross section, we take the incoherent approximation where S_d is set equal to zero in Eq. 2. Based on this assumption, Eq. 1 is developed to give (e.g., see Ref. [3]):

$$\frac{d^2\sigma}{dE d\Omega} = \frac{1}{4\pi} \frac{k'}{k} \left(\sigma_{\text{inelab}} S_d(\vec{k}, \omega) + \sigma_{\text{inelab}} S_d(\vec{k}, \omega) \right), \quad (1)$$

$$\frac{d^2\sigma}{dE d\Omega} = \frac{1}{4\pi} \frac{k'}{k} (\sigma_{\text{inelab}} + \sigma_{\text{inelab}}) S_d(\vec{k}, \omega). \quad (2)$$

However, for some important neutron materials such as graphite and beryllium, this assumption can introduce

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On a measurement approach to support evaluation of thermal scattering law data

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1. Introduction

Over the past 15 years, a general methodology has been developed to generate thermal neutron scattering law (TSL) data, and calculate the thermal neutron scattering cross sections for materials under various conditions and while retaining many of the traditional approximations (e.g., the incoherence approximation) that have been used for decades. This methodology uses molecular dynamics (MD) and density functional theory (DFT) approaches to calculate the scattering law and cross sections for TSL calculations, such as the atomic and molecular systems' extension to the thermal neutron scattering law. The data is accessed from the atomistic simulations and the resulting atomic correlations. In this case, corrections are needed to account for missing scattering terms due to the finite size of the atomistic model. This methodology has resulted in the largest contribution (in the last 5 years) to the development of the ENDF/B-VI nuclear data library (Browne, 2003).

In this paper, the motivation that would be the subject of the evolution process is originated from the fundamental equations of the double differential thermal scattering cross section. This formulation is derived using the first Born approximation of scattering theory. Then, the scattering law is calculated for the material known as the Fermi pseudopotential (e.g., see Ref. Squires, 1973). The following expression is obtained for the double differential thermal scattering cross section:

$$\frac{d^2\sigma}{d\Omega dE} = \frac{1}{4\pi k^2} \frac{\vec{k}}{k} \cdot \vec{S}(\vec{k}, \omega) \bar{S}(\vec{k}, \omega) + m_n S(\vec{k}, \omega) \quad (1)$$

$$S(\vec{k}, \omega) = S_d(\vec{k}, \omega) + S_{\text{inelab}}(\vec{k}, \omega) \quad (2)$$

$$\bar{S}(\vec{k}, \omega) = \int_0^\infty dE' \omega' \frac{1}{E'} \bar{S}(\vec{k}, \omega') + m_n S(\vec{k}, \omega) \quad (3)$$

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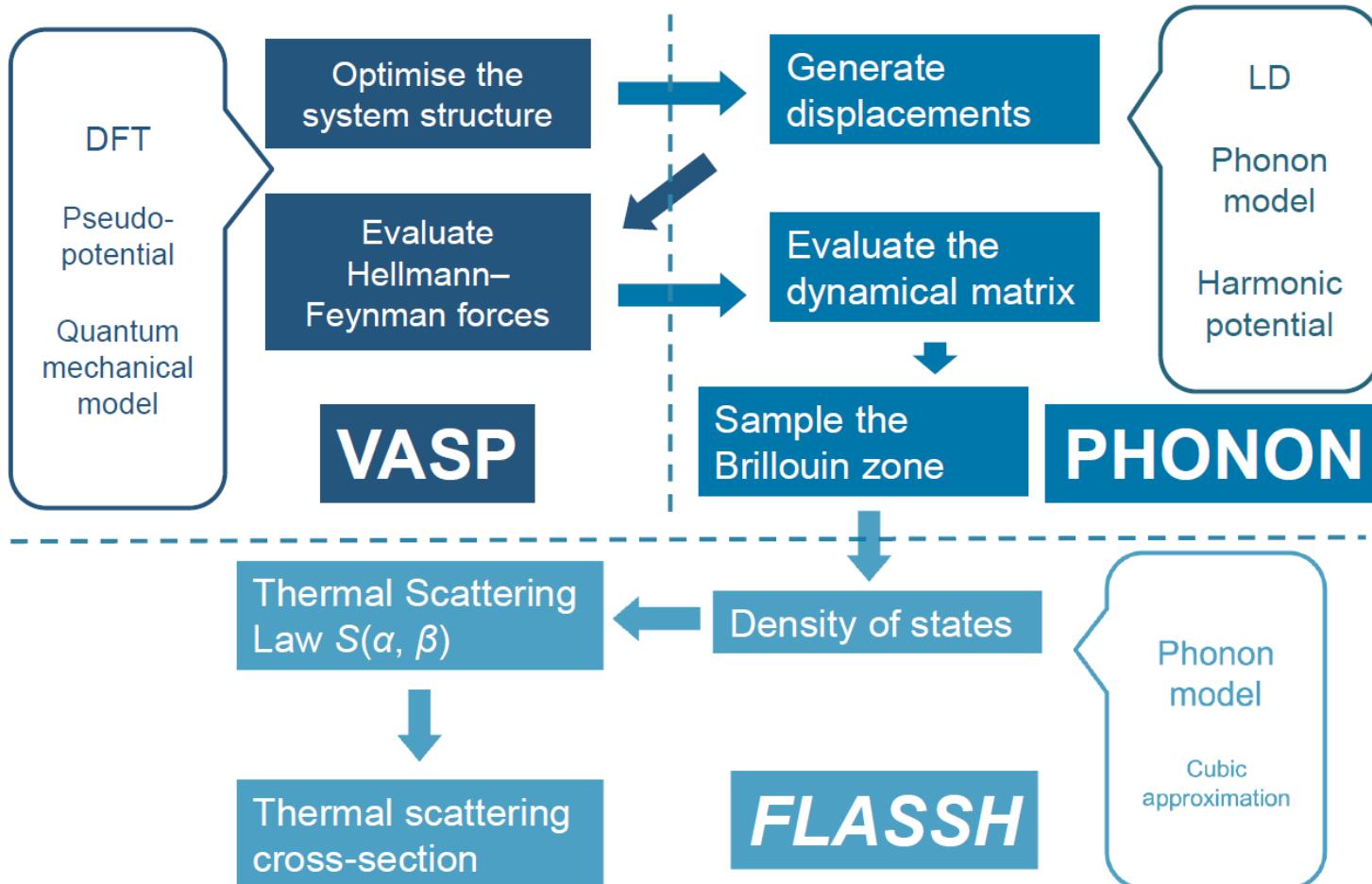
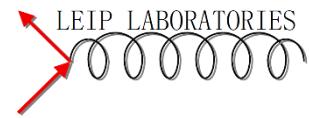
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Analysis Approach

- Construct atomistic model of a material
- Verify ability of model to reproduce physical properties of the material (equilibrium conditions)
 - Density, thermal expansion, thermal conductivity,...
 - Ergodic behavior, correlations,...
- Generate input (DOS, ...) for TSL calculations
- Calculate TSL and produce thermal scattering cross sections
 - Check consistency of results with computational assumptions/models
 - Compare to experimental data

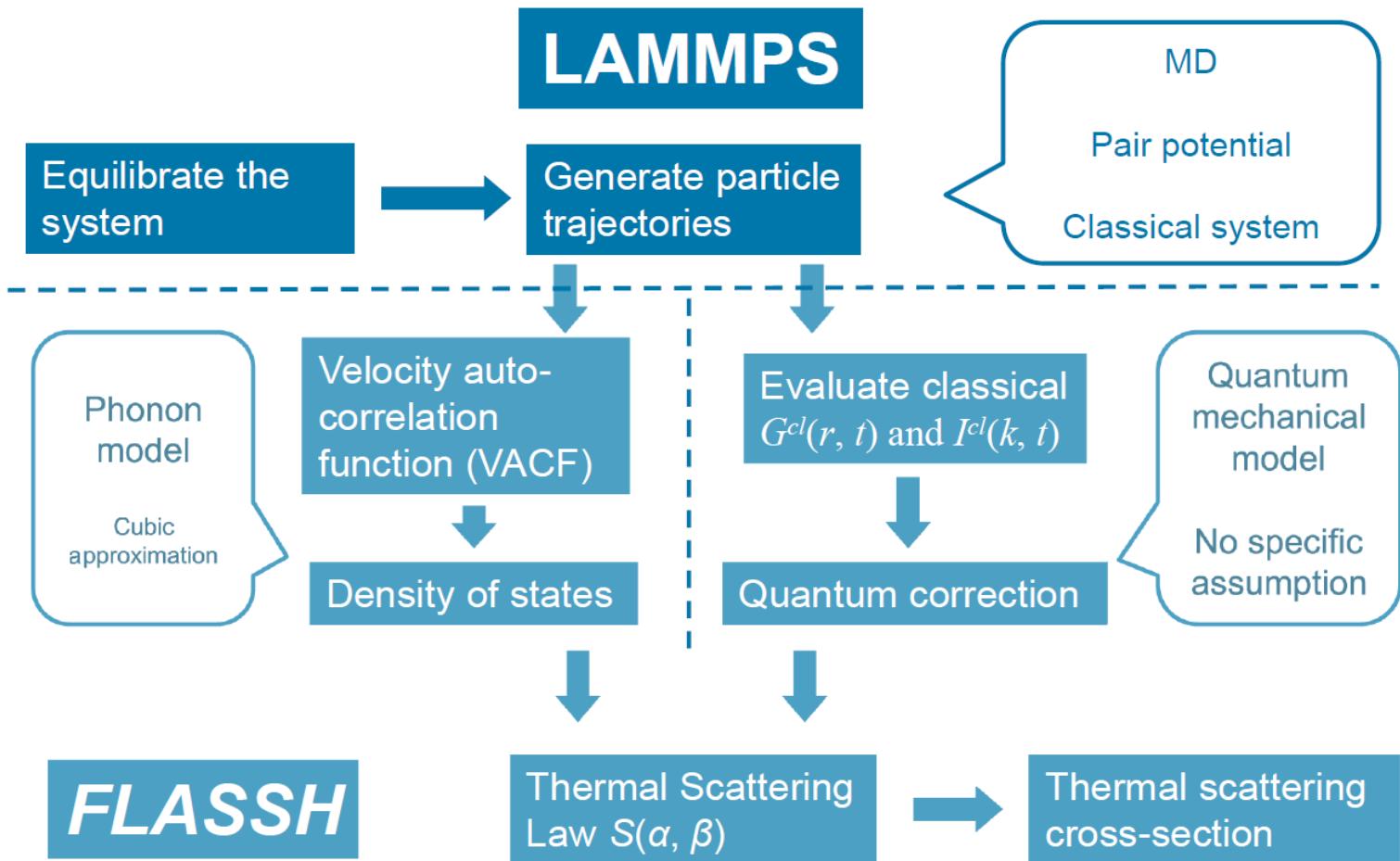
Thermal Scattering Law

DFT/LD



Thermal Scattering Law

MD/QM



ENDF/B-VIII TSL Evaluations

Material	ENDF Library Name	Evaluation Basis	Institution
Beryllium metal	tsl-Be-metal.endf	DFT/LD	NCSU
Beryllium oxide (beryllium)	tsl-BeinBeO.endf	DFT/LD	NCSU
Beryllium oxide (oxygen)	tsl-OinBeO.endf	DFT/LD	NCSU
Light water (hydrogen)	tsl-HinH2O.endf	MD	CAB
Light water ice (hydrogen)	tsl-HinIceIh.endf	DFT/LD	BAPL
Light water ice (oxygen)	tsl-OinIceIh.endf	DFT/LD	BAPL
Heavy water (deuterium)	tsl-DinD2O.endf	MD	CAB
Heavy water (oxygen)	tsl-OinD2O.endf	MD	CAB
Polymethyl Methacrylate (Lucite)	tsl-HinC5O2H8.endf	MD	NCSU
Polyethylene	tsl-HinCH2.endf	MD	NCSU
Crystalline graphite	tsl-graphite.endf	MD	NCSU
Reactor graphite (10% porosity)	tsl-reactor-graphite-10P.endf	MD	NCSU
Reactor graphite (30% porosity)	tsl-reactor-graphite-30P.endf	MD	NCSU
Silicon carbide (silicon)	tsl-CinSiC.endf	DFT/LD	NCSU
Silicon carbide (carbon)	tsl-SiinSiC.endf	DFT/LD	NCSU
Silicon dioxide (alpha phase)	tsl-SiO2-alpha.endf	DFT/LD	NCSU
Silicon dioxide (beta phase)	tsl-SiO2-beta.endf	DFT/LD	NCSU
Yttrium hydride (hydrogen)	tsl-HinYH2.endf	DFT/LD	BAPL
Yttrium hydride (yttrium)	tsl-YinYH2.endf	DFT/LD	BAPL
Uranium dioxide (oxygen)	tsl-OinUO2.endf	DFT/LD	NCSU
Uranium dioxide (uranium)	tsl-UinUO2.endf	DFT/LD	NCSU
Uranium nitride (nitrogen)	tsl-NinUN.endf	DFT/LD	NCSU
Uranium nitride (uranium)	tsl-UinUN.endf	DFT/LD	NCSU

ENDF/B-VIII TSL Evaluations

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Beryllium oxide (oxygen)	tsl-OinBeO.endf	DFT/LD	NCSU
Light water (hydrogen)	tsl-HinH2O.endf	MD	CAB
Light water ice (hydrogen)	tsl-HinIceIh.endf	DFT/LD	BAPL
Light water ice (oxygen)	tsl-OinIceIh.endf	DFT/LD	BAPL
Heavy water (deuterium)	tsl-DinD2O.endf	MD	CAB
Heavy water (oxygen)	tsl-OinD2O.endf	MD	CAB
Polymethyl Methacrylate (Lucite)	tsl-HinC5O2H8.endf	MD	NCSU
Polyethylene	tsl-HinCH2.endf	MD	NCSU
Crystalline graphite	tsl-graphite.endf	MD	NCSU
Reactor graphite (10% porosity)	tsl-reactor-graphite-10P.endf	MD	NCSU
Reactor graphite (30% porosity)	tsl-reactor-graphite-30P.endf	MD	NCSU
Silicon carbide (silicon)	tsl-CinSiC.endf	DFT/LD	NCSU
Silicon carbide (carbon)	tsl-SiinSiC.endf	DFT/LD	NCSU
Silicon dioxide (alpha phase)	tsl-SiO2-alpha.endf	DFT/LD	NCSU
Silicon dioxide (beta phase)	tsl-SiO2-beta.endf	DFT/LD	NCSU
Yttrium hydride (hydrogen)	tsl-HinYH2.endf	DFT/LD	BAPL
Yttrium hydride (yttrium)	tsl-YinYH2.endf	DFT/LD	BAPL
Uranium dioxide (oxygen)	tsl-OinUO2.endf	DFT/LD	NCSU
Uranium dioxide (uranium)	tsl-UinUO2.endf	DFT/LD	NCSU
Uranium nitride (nitrogen)	tsl-NinUN.endf	DFT/LD	NCSU
Uranium nitride (uranium)	tsl-UinUN.endf	DFT/LD	NCSU

Thermal Scattering Law Analysis

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Ab Initio Generation of Thermal Neutron Scattering Cross Sections

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Raleigh, NC 27695-7809

Quantum mechanics ab initio (i.e., first principle) methods are applied in generating the thermal neutron scattering cross sections of model materials and reflectors that are of interest in nuclear technology. Specifically, this work focuses on graphite and beryllium. In both cases, the ab initio code VASP and the lattice dynamics code PHONON were used to generate the dispersion relations, and the phonon frequency distributions (density of states) were used to find the total energy of the system. The code NJOY is used to calculate the thermal neutron scattering cross sections at various temperatures. The use of the ab initio approach represents a major departure from previously applied methods, which depended mainly on using simpler dynamical models to expand data to arrive at the phonon frequencies distributions. In this case, much more complicated details of the atomic system can be taken up, which allows the establishment of a more complete dynamical matrix. As opposed to the semi-empirical methods used previously, this method represents a fundamental and predictive approach for estimating materials' properties including ones that are of interest in nuclear reactor design.

KEYWORDS: neutron, thermal neutron, slow neutron, ab initio, VASP, graphite, beryllium, moderator, phonon frequency distribution, thermal neutron scattering cross section, nuclear reactor

1. Introduction

Due to advances in computational power, the possibility now exists to perform detailed quantum mechanical ab initio (i.e., first principle) calculations of atomic systems. These calculations are applied in generating the thermal neutron scattering cross sections of model materials and reflectors that are of interest in nuclear technology. Specifically, this work focuses on graphite and beryllium. In both cases, the ab initio code VASP and the lattice dynamics code PHONON were used to generate the dispersion relations, and the phonon frequency distributions (density of states) were used to find the total energy of the system. The code NJOY is used to calculate the thermal neutron scattering cross sections at various temperatures. The use of the ab initio approach represents a major departure from previously applied methods, which depended mainly on using simpler dynamical models to expand data to arrive at the phonon frequencies distributions. In this case, much more complicated details of the atomic system can be taken up, which allows the establishment of a more complete dynamical matrix. As opposed to the semi-empirical methods used previously, this method represents a fundamental and predictive approach for estimating materials' properties including ones that are of interest in nuclear reactor design.

In nuclear reactors, the effect of atoms on molecular bonding becomes important as the neutrons slow down and enter the thermal (or slow) region (neutron energy $\leq 1 \text{ eV}$). The microscopic interaction (i.e., absorption, scattering, etc.) of slow neutrons within the reactor core defines the thermal neutron energy spectrum, which affects several global (macroscopic) properties such as criticality, and safety and feedback response. Therefore, the accuracy of the thermal neutron scattering cross sections that are used in reactor core design calculations are important for operating the reactor in an optimum and safe manner.

In the past, the thermal neutron scattering cross sections were derived from atomic dynamics models that were fitted to experimental data in order to quantify the forces between the atoms and calculate the required excitation density of states [1]. However, by using the ab initio approach, the ability now exists to treat much larger systems of atoms, and arrive at more accurate and complete dynamical models from



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A predictive approach based on ab initio quantum mechanics and/or classical molecular dynamics simulations has been formulated to calculate the scattering law, $S(\vec{k}, \omega)$, and the thermal neutron scattering cross section, $\sigma_{\text{th}}(\vec{k}, \omega)$. This approach is based on the assumption that it is possible to generate the inelastic thermal neutron scattering cross section of any material and to accurately reflect the physical conditions of the medium (i.e., temperature, pressure, etc.). In addition, the present approach is based on the application of the principles of quantum mechanics and statistical thermodynamics theory, and, in the case of solids, crystalline perfection. As a result, a new and improved thermal neutron scattering analysis technique has been developed. This technique is based on the use of the atomic mass materials used for reactor moderators and reflectors such as reactor-grade graphite and beryllium. The present approach is based on the use of the atomic mass materials used for reactor moderators and reflectors such as graphite and neutron beam filters such as copper and bismuth. Consequently, it is anticipated that the above approach will play a major role in providing the nuclear science and engineering community with a new and improved technique for calculating the thermal neutron scattering cross sections of new materials when experimental information may be scarce or nonexistent.

1. INTRODUCTION

Low energy ($\leq 1 \text{ eV}$) thermal neutron scattering is characterized by the ratio of the order of magnitude between the incident energy and the energy in which they interact. Furthermore, they do Bragg wavelength in the solid state. In this case, the scattering law is characterized by the magnitude of the wave vector of the incident and scattered waves, \vec{k} , and the magnitude of the inelastic coherent scattering cross section, and σ_{th} is the bound state incoherent scattering cross section. In general, S is composed of two terms as follows

$$S(\vec{k}, \omega) = S_c(\vec{k}, \omega) + S_i(\vec{k}, \omega), \quad (2)$$

where S_c is known as the self-scattering law, which accounts for non-interference (incoherent) effects, while S_i is the inelastic thermal neutron scattering law (coherent) effects. Examination of Eq. (2) shows that the thermal neutron scattering cross section depends on the inelastic scattering cross section, σ_{th} , which is represented by the bound atom cross sections, and second, a factor that represents the dynamics of the scattering, namely, the scattering law, $S(\vec{k}, \omega)$, which is given by the scattering law, $S(\vec{k}, \omega)$.

The calculation of the double differential scattering cross section inside the incoherent approximation where S_i is set equal to zero in Eq. 2. Based on this assumption, Eq. 2 is developed to give (e.g., Ref. [2])

$$\frac{d^2\sigma}{dE d\Omega} = \frac{1}{4\pi} \frac{k'}{4\pi} [\sigma_{\text{th}} + \sigma_{\text{incoh}}] S_c(\vec{k}, \omega). \quad (1)$$

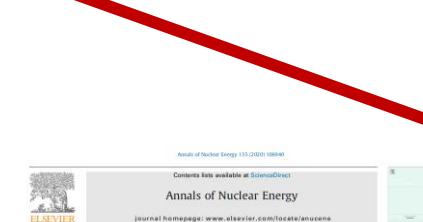
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$$\frac{d^2\sigma}{dE d\Omega} = \frac{1}{4\pi} \frac{k'}{4\pi} [\sigma_{\text{th}} + \sigma_{\text{incoh}}] S_c(\vec{k}, \omega). \quad (3)$$

However, for some important neutronic materials such as graphite and beryllium, this assumption can introduce



On a measurement approach to support evaluation of thermal scattering law data

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ABSTRACT

Inelastic thermal neutron scattering in materials that act as neutron moderators, reflectors, and filters is important for the safe operation of nuclear reactors. This paper discusses the development of inelastic thermal neutron scattering cross sections from three components that include the bound atom (i.e., incoherent scattering law), the inelastic thermal neutron scattering law (i.e., $S_c(\vec{k}, \omega)$), and the double differential thermal neutron scattering cross section, $\sigma_{\text{th}}(\vec{k}, \omega)$. However, valuable information may be derived from measurements and "targeted" experiments that are designed to support the evaluation of the thermal neutron scattering law. In addition, the correlation of confirmed measurements and experiments is described that was designed and used to support the evaluation of the TSL for "nuclear graphite". This experimental suite includes neutron powder diffraction (measuring the incoherent scattering law), neutron scattering (measuring the double differential thermal neutron scattering cross section), and neutron transmission (measuring the double differential thermal neutron scattering cross section). The correlation of these three experiments and the use of the double differential thermal neutron scattering cross section in the ENDF-VIII nuclear data library release is shown to provide a significant improvement in the quality of the thermal neutron scattering cross section of "nuclear" graphite in the ENDF-VIII nuclear data library release.

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1. Introduction

Over the past 15 years, a general methodology has been developed to generate thermal neutron scattering law (TSL) data, and catalog them in the ENDF-VIII nuclear data library. This is done for materials under various conditions and while retaining many of the features of the previous ENDF-VII nuclear data library (Hawari, 2014, 2004). The methodology is based on using molecular dynamics (MD) and/or quantum mechanics (QM) simulation methods to derive the fundamental input needed for TSL calculations, such as the atomic and molecular system's excitation energy, density of states, and the scattering law. This is accessed from the atomic simulations and the resulting atomic scattering cross sections. The TSL data is generated by fitting the last 50 years of TSL data to the recently released ENDF-VIII nuclear data libraries (Brown, 2010).

In this paper, we would like to be the subject of the evaluation process originates from the fundamental equations for

the double differential thermal scattering cross section. This formalism is based on the double differential thermal scattering theory and assumes a highly localized nuclear potential known as the Fermi pseudopotential (e.g., see Ref. Scopigno, 1975; Scopigno et al., 1975). This is the same formalism used for the double differential thermal scattering cross section

$$\frac{d^2\sigma}{dE d\Omega} = \frac{4\pi k'}{4\pi} \left[\sigma_{\text{th}} S_c(\vec{k}, \omega) + \sigma_{\text{incoh}} S_i(\vec{k}, \omega) \right], \quad (1)$$

$$S(\vec{k}, \omega) = S_c(\vec{k}, \omega) + S_i(\vec{k}, \omega), \quad (2)$$

where, $S(\vec{k}, \omega)$ is the thermal scattering law, $S_c(\vec{k}, \omega)$ is the distinct scattering law, ω , and k' are dimensionless variables. σ_{th} is the inelastic bound state cross section, σ_{incoh} is the incoherent bound state cross section, ω is the scattering wave number, E is the scattered neutron energy, Ω is the scattering solid angle, k is Boltzmann's constant, and T is the temperature of the scattering source. The double differential thermal scattering cross section is the product of the double differential thermal scattering cross section and the density distribution function for an atom at a given time and of the density distribution function for an atom at a given initial location in the atomic system with its location at time t . S_i is related to the Fourier transform in space and time of the density

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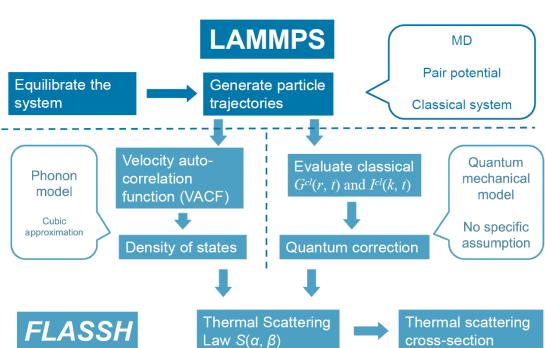
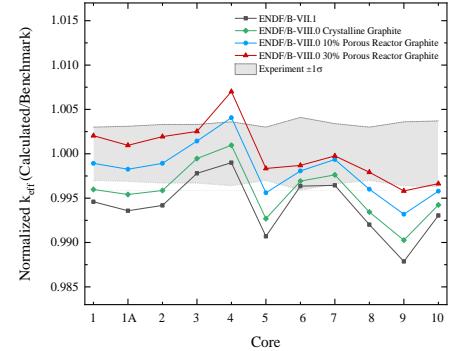
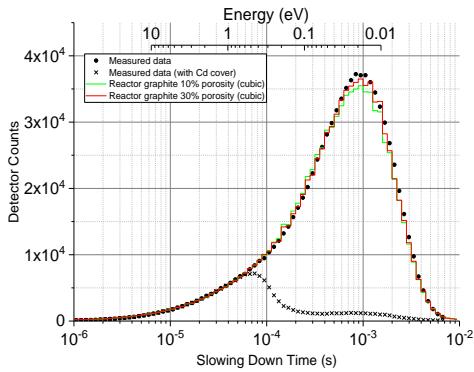
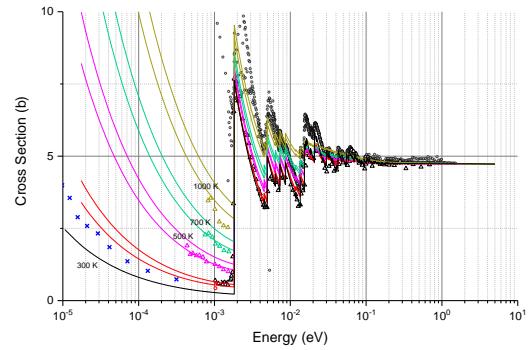
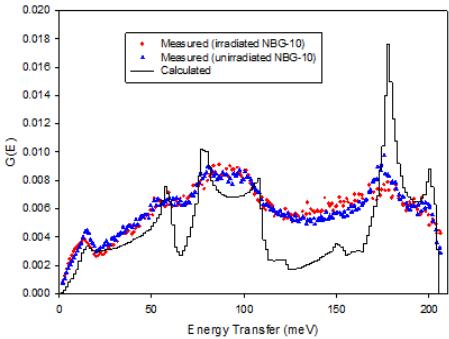
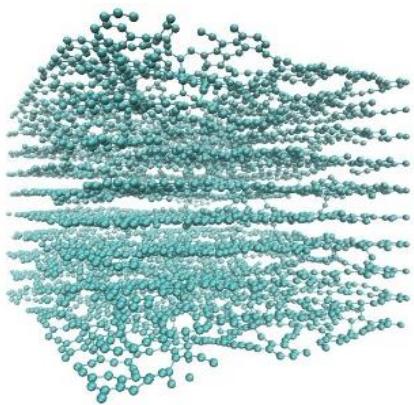
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Nuclear Graphite



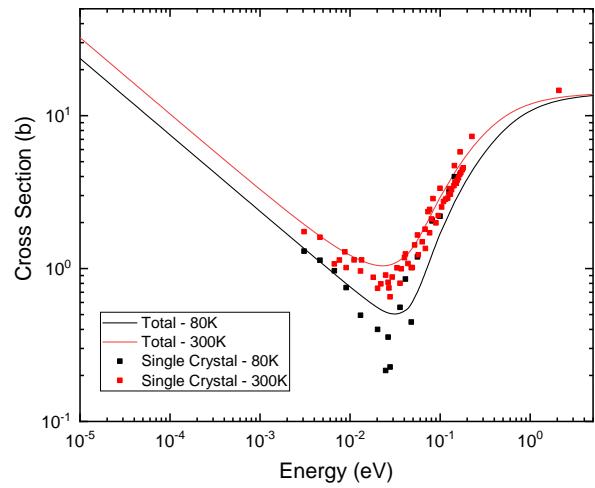
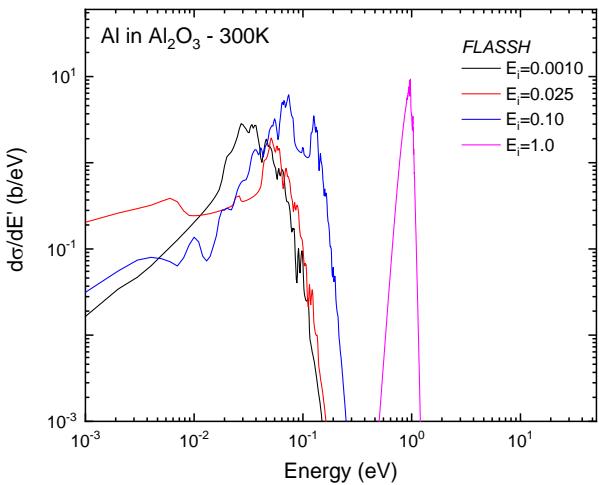
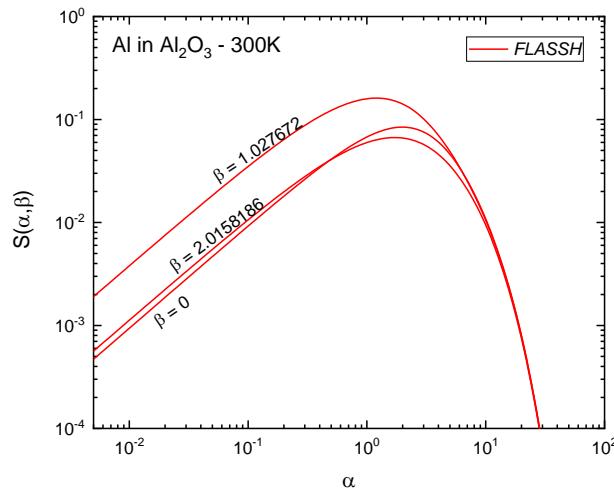
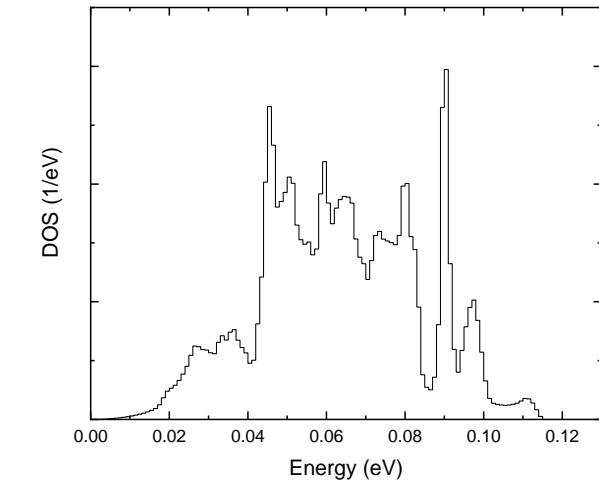
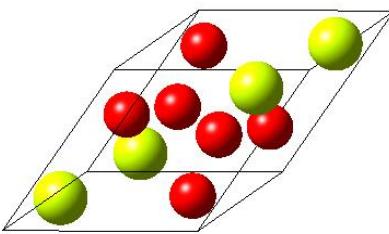
Evaluation

Measurements/Benchmarks

New to NNDC

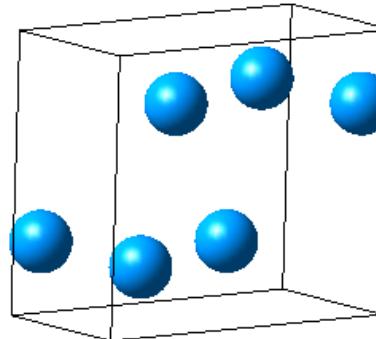
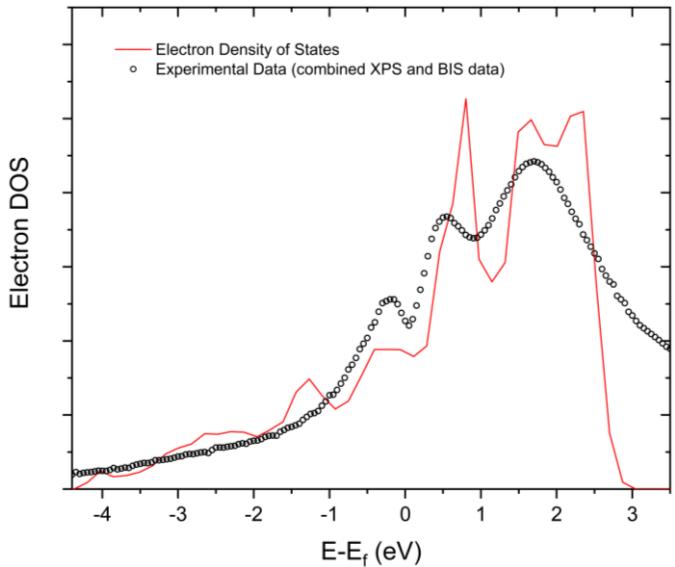
Single Crystal Sapphire TSL Data

- ▶ *Ab initio* lattice dynamics
 - Predictive density of states (DOS)
 - Rhombohedral structure
 - 2x2x2 supercell
 - GGA-PBE



Uranium Metal

- ▶ α -Uranium Metal
 - ▶ Stable up to 668°C
- ▶ *Ab initio* lattice dynamics
 - ▶ DFT – GGA-PBE plus an effective Coulomb term (+U) of 1eV for the 5f electrons plus spin-orbit coupling

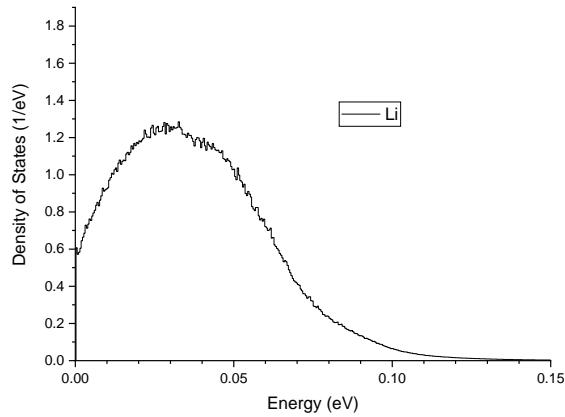


- Orthorhombic structure
- 550 eV plane wave cutoff
- 12x12x7 k-mesh

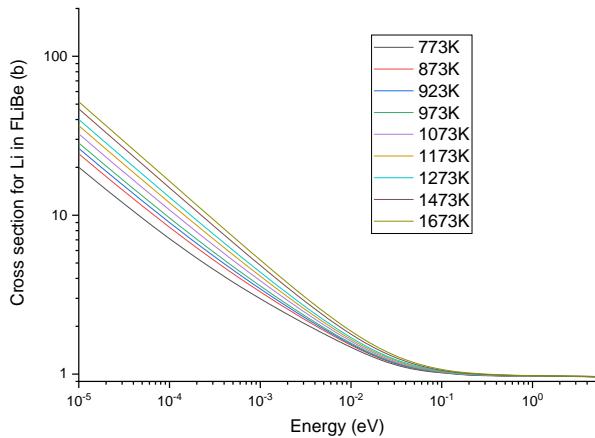
	Experiment (4.2 K)	Calculated	Diff. (%)
a (Å)	2.8444	2.8565	0.42
b (Å)	5.8689	5.8706	0.03
c (Å)	4.9316	4.9834	1.05

Completed FLiBe TSL Data

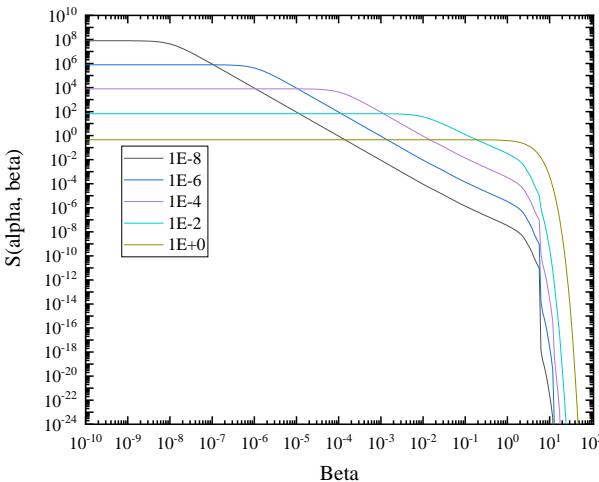
DOS using MD 773 K



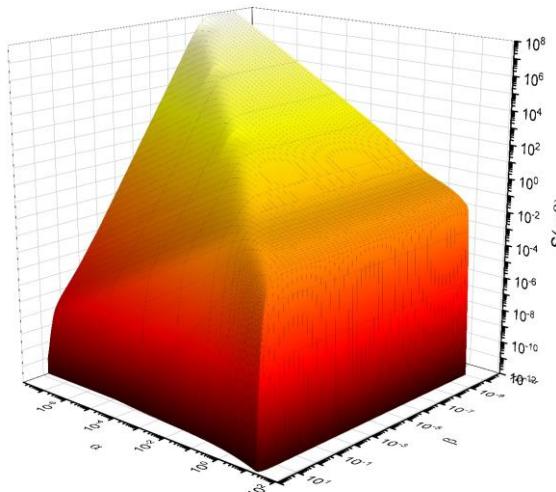
Cross section using *FLASHH*



TSL using *FLASHH* 773 K

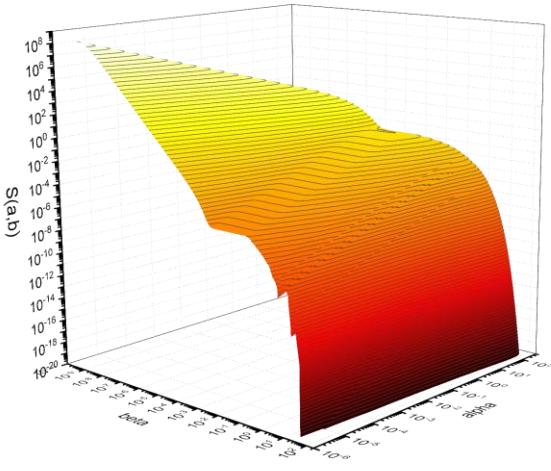
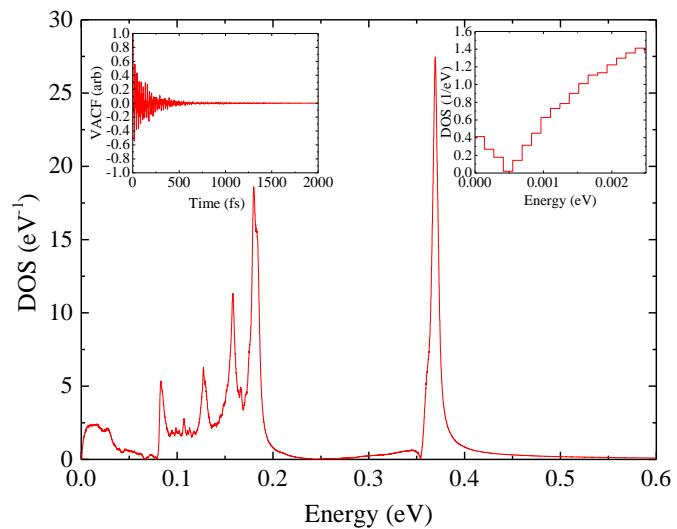
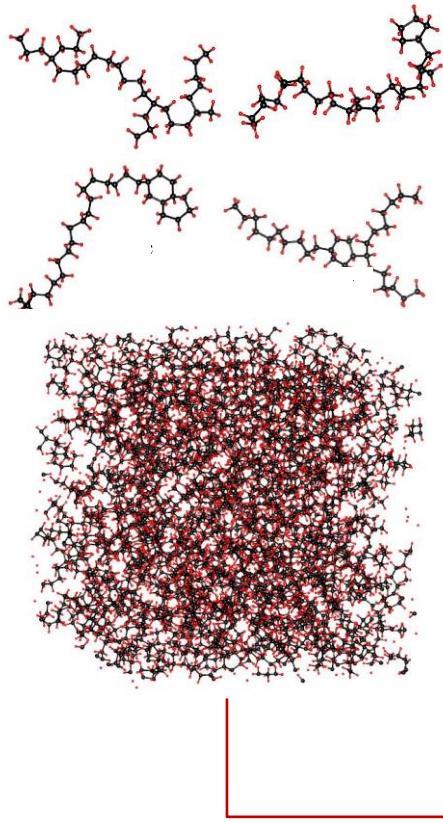


TSL using *FLASHH* 773 K



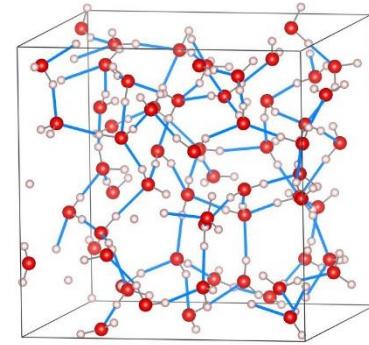
New to NNDC

Heavy Paraffinic Oil

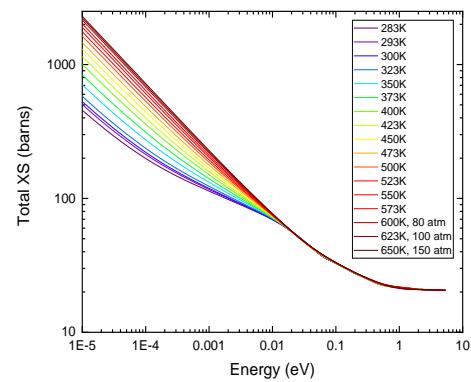
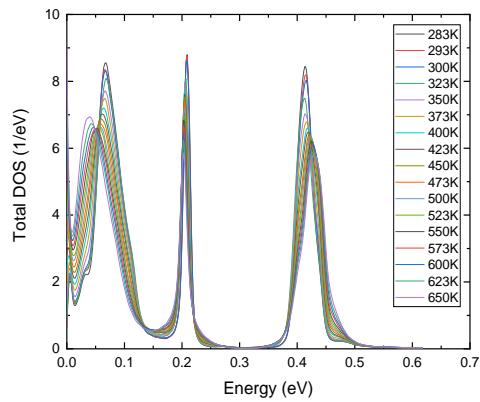
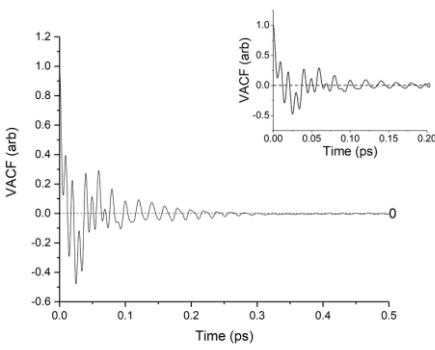


Light Water TSL Data

- Flexible TIP4P/2005 potential
- Molecular dynamics model
 - LAMMPS code
 - 1000 molecules

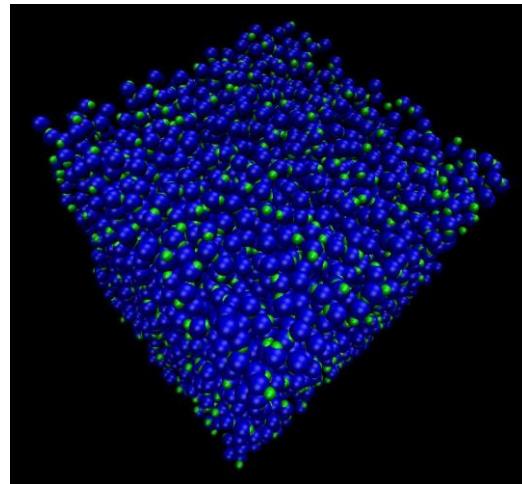


$$U^{tot} = U^{\text{inter}} + U^{\text{intra}} = \sum_{i \neq j} 4\epsilon \left[\left(\frac{\sigma}{r_{O_i O_j}} \right)^{12} - \left(\frac{\sigma}{r_{O_i O_j}} \right)^6 \right] + \sum_{i \neq j} \frac{q_i q_j}{r_{ij}} + D_r \left\{ 1 - \exp \left[-\beta(r_{OH} - r_{eq}) \right] \right\}^2 + \frac{1}{2} K_\theta (\theta - \theta_{eq})^2$$

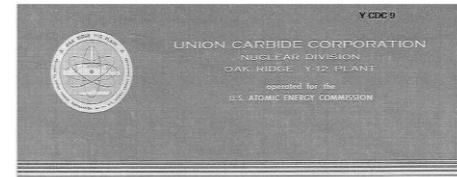


Hydrofluoric Acid MD

- Constructed potential function
- Molecular dynamics model
 - LAMMPS code
 - 4000 molecules

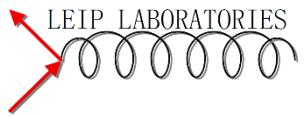


$$U^{total} = \sum_i \frac{1}{2} k_D |\mathbf{r}_{F,i} - \mathbf{d}_i|^2 + \frac{1}{2} k_{HF} (r_{HF} - d_{FH})^2 + \sum_{i < j} \sum_{s,\dot{s}} \frac{q_s q_{\dot{s}}}{|\mathbf{r}_{s,i} - \mathbf{r}_{\dot{s},i}|} + \sum_{i < j} 4 \varepsilon_{FF} \left[\left(\frac{\sigma_{FF}}{|\mathbf{r}_{F,i} - \mathbf{r}_{F,j}|} \right)^{12} - \left(\frac{\sigma_{FF}}{|\mathbf{r}_{F,i} - \mathbf{r}_{F,j}|} \right)^6 \right]$$



- Testing is underway using experimental data derived from
“CRITICALITY OF LIQUID MIXTURES OF HIGHLY 235U-ENRICHED URANIUM HEXAFLUORIDE AND HYDROFLUORIC ACID”





FLASSH Code

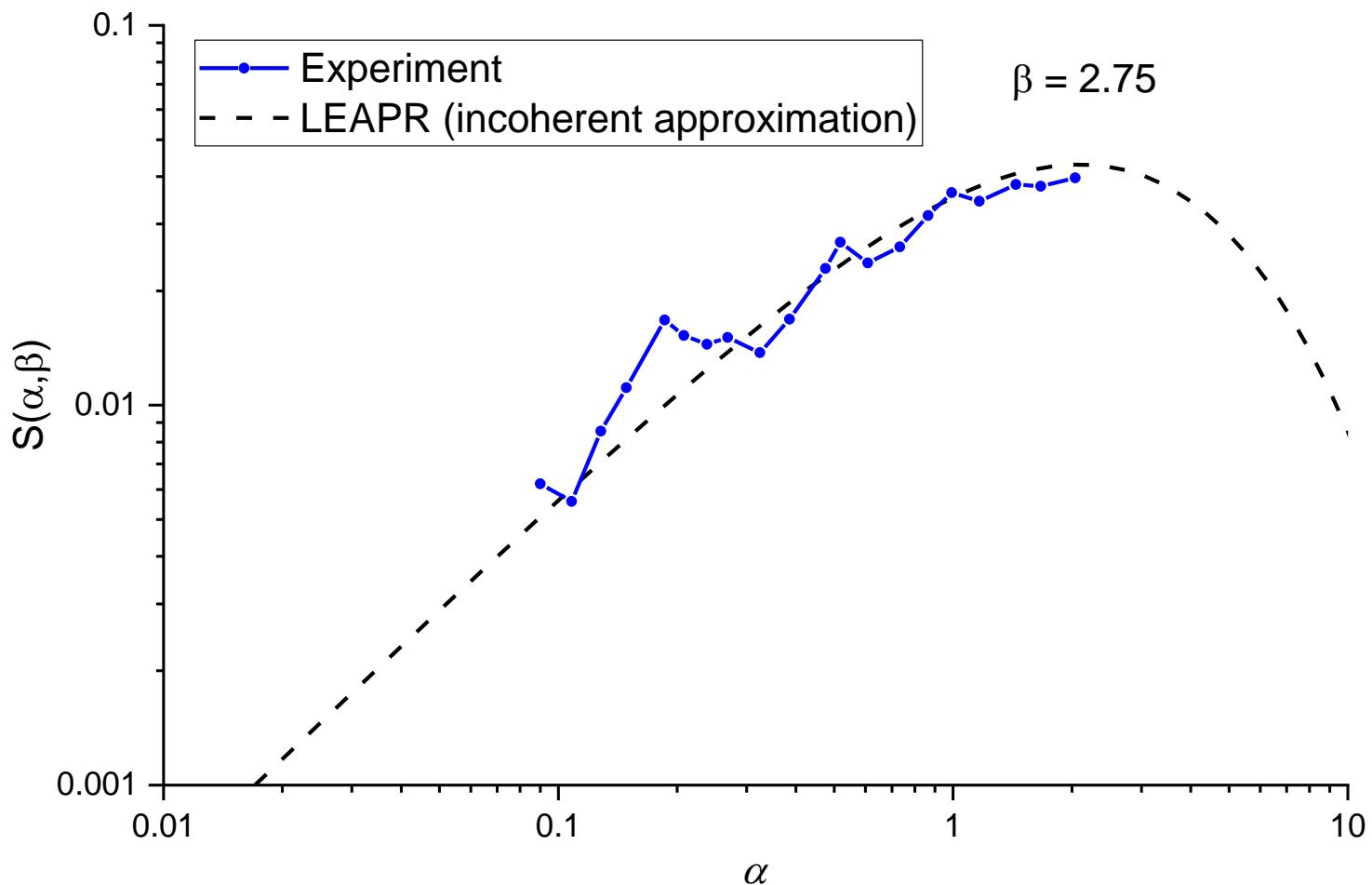
- *FLASSH* Code
 - Relaxed major approximations (incoherent, cubic, ect.)
 - Improved liquid physics
 - Improved Output Formatting
 - Warning Messages for the User
- *FLASSH* GUI
 - Error Checks
 - Crystal Structure Window/Inputs
 - ENDF Header Formatting

The image shows the FLASSH GUI interface. The top window is titled "Crystal Structure: U_UN" and contains fields for "Material Selection" (set to "12 - U in UN"), "Parameters [a b c [Å] α β γ [°] (space group)]: 4.85945 4.85945 4.85945 90 90 90 (Fm-3m)", and "Input unit cell vectors a, b, and c, in the unit of Å." A table provides these vectors:

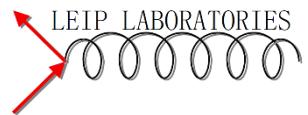
	X	Y	Z
a	4.85945	0.00000	0.00000
b	0.00000	4.85945	0.00000
c	0.00000	0.00000	4.85945

The bottom window is titled "FLASSH: U_UN" and shows the FLASSH logo and "Full Law Analysis Scattering System Hub". It includes tabs for "Project", "Create", "Run", and "Help". The copyright notice "Do not distribute without explicit permission from Ayman Hawari (aihawari@ncsu.edu)" is visible at the bottom of the main window. The LEIP LABORATORIES logo is also present at the bottom of the main window.

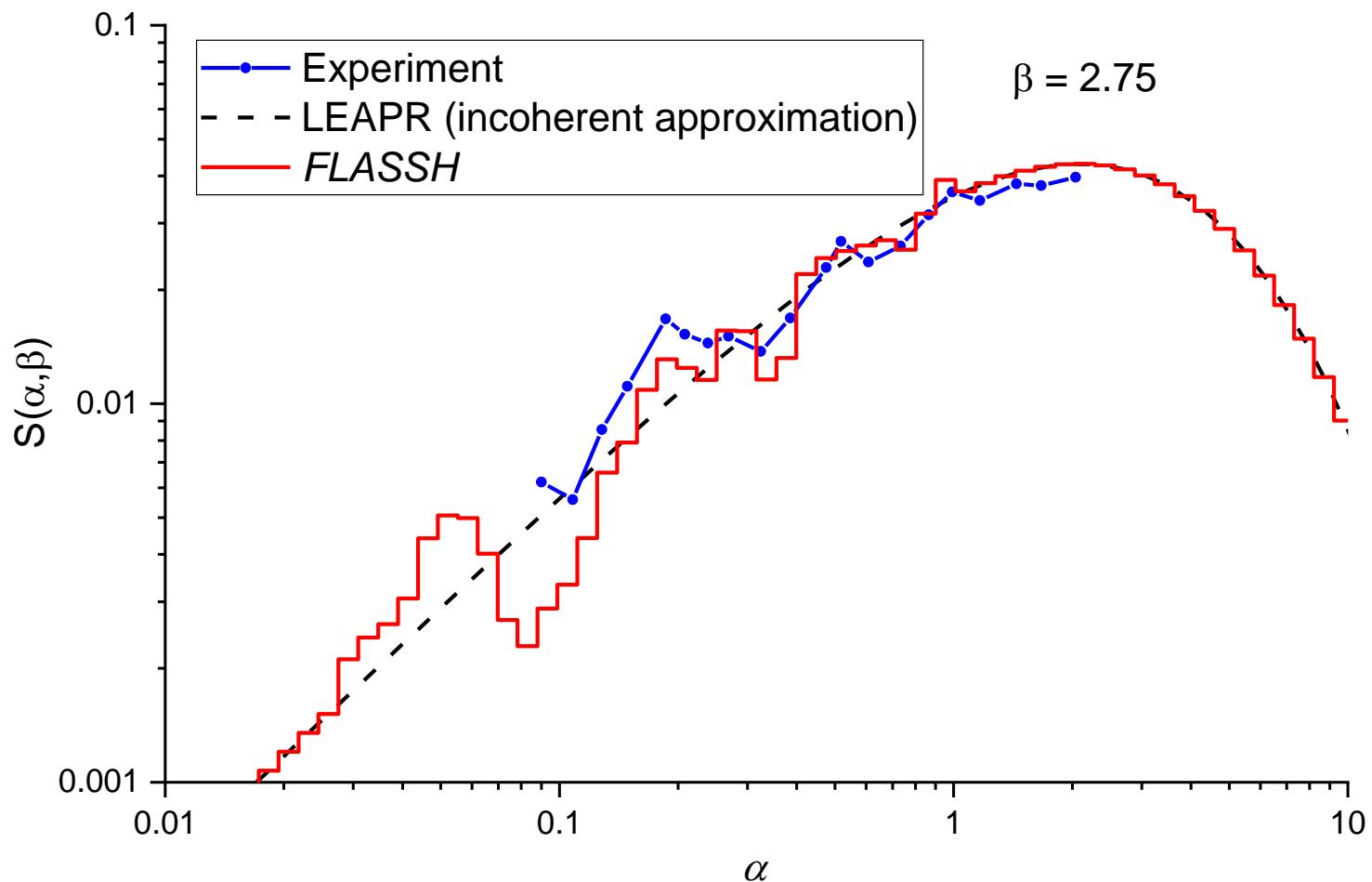
NJOY

Be Scattering Law $S(\alpha, \beta)$ 

FLASSTH



Be Scattering Law $S(\alpha, \beta)$



FLASSTH – Generalized TSL & Doppler Treatment

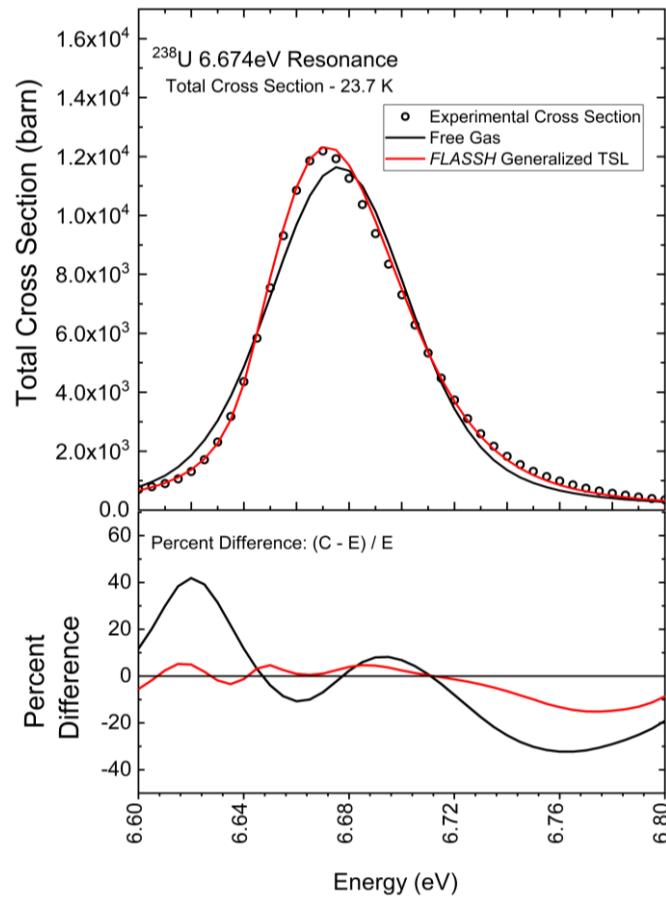
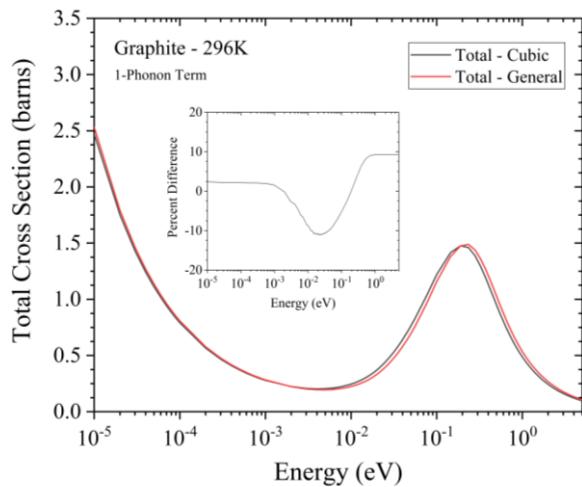
□ Generalized TSL

- Exact Structure
- Polarization vectors and frequencies directly input
- Removes cubic and atom site approximation

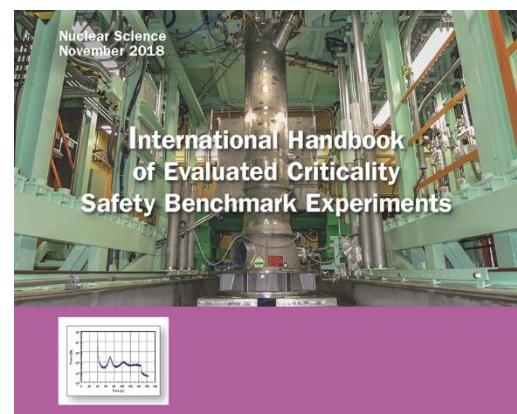
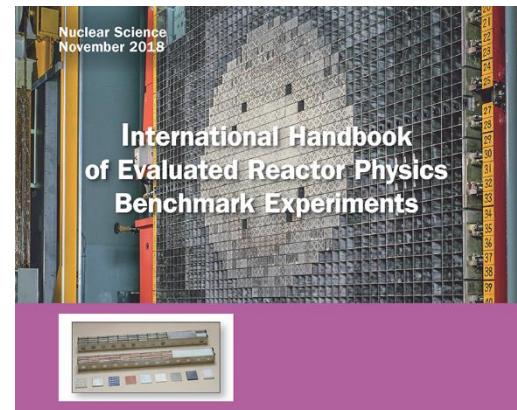
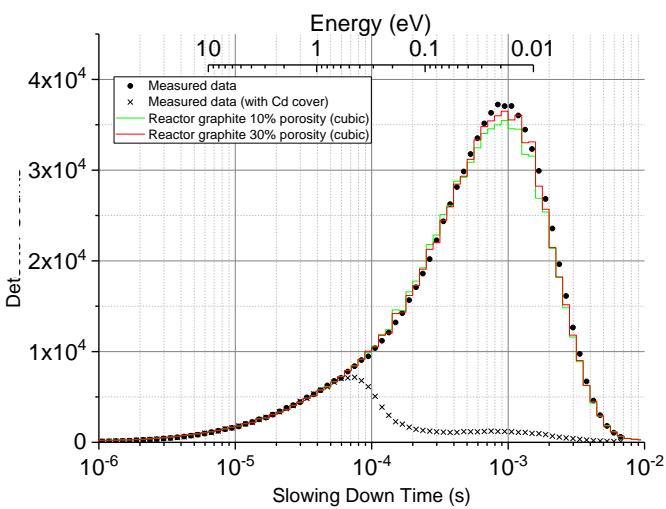
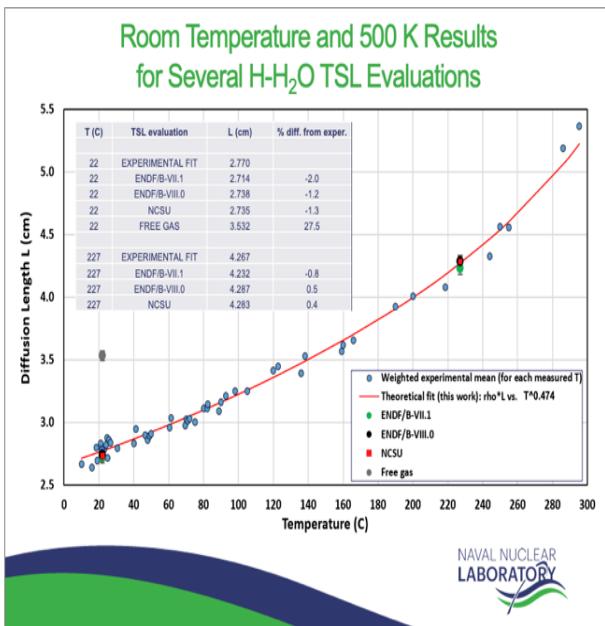
□ Doppler Broadening

- *FLASSTH* TSL to determine velocity distribution for broadening
- Implements exact material structure
- Consistent evaluation for both thermal scattering and Doppler broadening

$$\begin{aligned} S_s^m(k, \omega) &= \int e^{-i\omega t} I_s^m(k, t) dt \\ &= \int e^{-i\omega t} e^{\langle U^2 \rangle_m + \langle UV_0 \rangle_m} dt \end{aligned}$$



TSL Specific Benchmarks



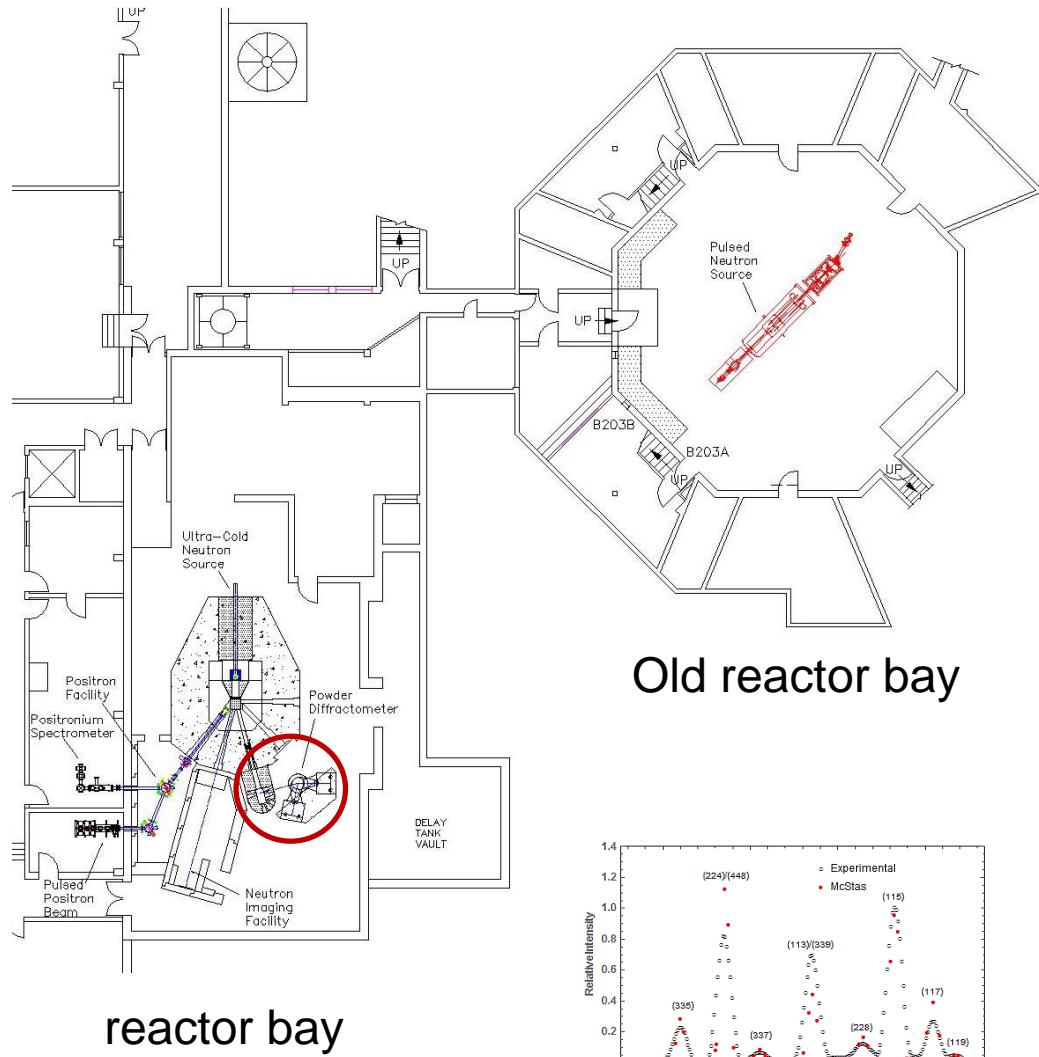
PULSTAR reactor

□ Current major facilities/capabilities

- **Neutron powder diffraction**
- Neutron imaging
- Intense positron beam
- Ultracold neutron source (under testing)
- Neutron activation analysis
- In-pool irradiation testing facilities

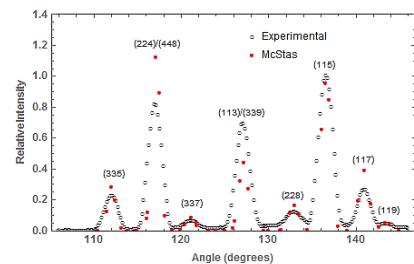
□ Current projects

- PULSTAR power upgrade 1-2 MW (licensing stage)
- Various instrument and facility upgrades
- **Pulsed accelerator neutron source (under testing)**
- Fuel loop for fission gas release studies



Old reactor bay

reactor bay



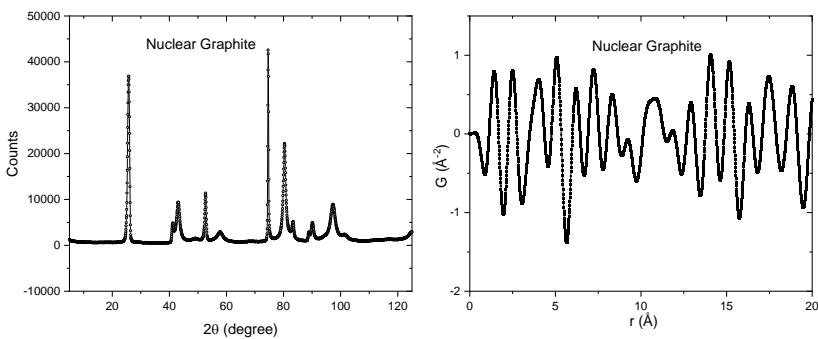
Cross Section Measurement Project

NPDF Facility Upgrades –
Dual Purpose:

- Diffraction Measurements:
15 New Position Encoding Modules (PEM) – improved diffraction measurement resolution $\Delta d/d$ of 2.9×10^{-3} for 3mm holder

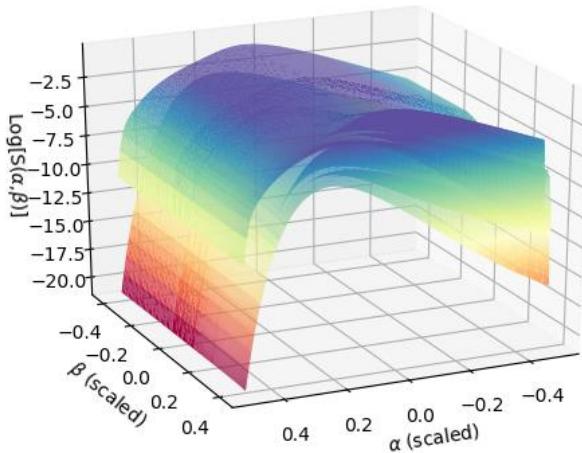
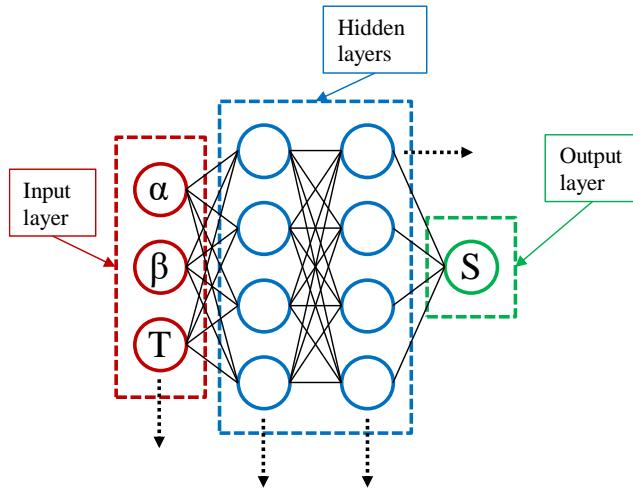
□ Transmission Measurement Capabilities:

- Monochromator capable of providing beam wavelengths of 1.085 \AA , 1.180 \AA , 1.479 \AA , and 1.762 \AA
- Transmission Detection Apparatus with collimator.



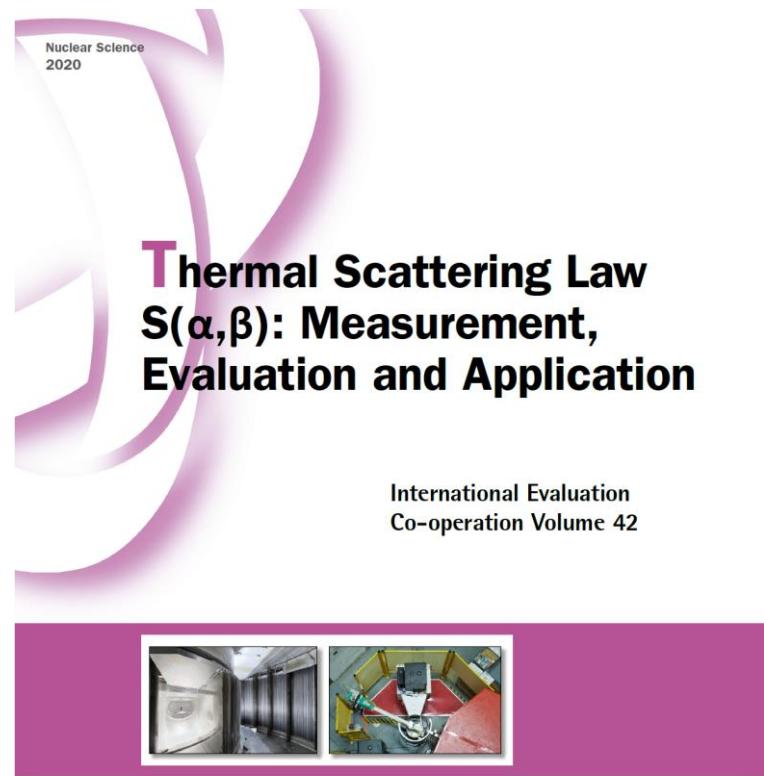
TSL NeTS

- New TSL paradigm
 - DL Neural Thermal Scattering (NeTS) modules
- See papers and presentations
 - ANS 2019 Winter Meeting, Washington, DC, USA
 - PHYSOR 2020 Meeting, Cambridge, UK



OECD/NEA WPEC Subgroup 48

- Kick-off in May 2020 during WPEC meeting
 - Motivate the TSL evaluation effort in support of various nuclear science and engineering applications
 - Advanced reactors (e.g., various molten salts)
 - Criticality safety (e.g., various U and Pu based fuels)
 - Neutron science (e.g., cryogenic moderators)
 - Review the development of advanced TSL evaluation methods and tools with consideration of modern simulation approaches
 - Address issues related to data validation, covariance generation, and data formats, ...



Summary

- ❑ TSL Activities continue including evaluations and methods development
- ❑ Evaluations are contributed to NNDC
 - Paraffinic oil and single crystal sapphire
 - Molten salt FLiBe will be submitted soon
 - Reevaluation of light water is ongoing
 - Hydrofluoric acid is initiated
 - Uranium metal is initiated
- ❑ *FLASSH* testing and several evaluations are underway
- ❑ Activities in data measurements and benchmark development are underway
- ❑ DL NeTS approach is under testing